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Nota di contenuto	Cover -- Half Title -- Title Page -- Copyright Page -- Contents -- Contributors -- Blue-Ribbon Panel Reviewers -- Acknowledgments -- Preface -- Chapter 1 : Introduction -- Chapter 2 : Predesign Surveys -- 2.1 Introduction -- 2.2 Surface Survey -- 2.3 Subsurface Investigation -- 2.3.1 Utility Research -- 2.3.1.1 Pipe Locators. Utility lines can have both horizontal and vertical locations identified by means of surface-applied pipe locators. Pipe locators can be instruments that simply detect underground lines by means of a magnetic field application -- 2.3.1.2 Ground-Penetrating Radar. Ground-penetrating radar (GPR) utilizes radio waves to detect underground lines and surfaces. When an object is detected, the radio waves reflect back to the receiver that records the information. The data are down -- 2.3.1.3 Vacuum Excavation. Nondestructive vacuum excavation is used to physically remove soil and expose the utility lines being investigated. Unlike test pits, which are completed by means of excavation equipment such as a backhoe, vacuum excavati -- 2.3.1.4 Seismic Surveys. Seismic surveys require that a small explosive charge or impact by means of sledgehammer be initiated and detected via a series of detectors or geophones spaced along the path of the utility line. A time recorder is used to -- 2.3.2 Geotechnical Investigation -- References -- Chapter 3 : Drilled Path Design -- 3.1 Introduction -- 3.2 Penetration Angles -- 3.3 Depth of Cover -- 3.4

Elevations of Entry and Exit -- 3.5 Radius of Curvature -- 3.6  
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 Method -- 3.8 Multiple-Line Installations -- 3.9 Utility Casings --  
 3.10 Annular Seepage -- References -- Chapter 4 : Pipe Design --  
 4.1 Introduction -- 4.2 Installation Loads -- 4.2.1 Tension.  
 4.2.1.1 Frictional Drag. Frictional drag between the pipe and the  
 soil is determined by multiplying the bearing force that the pull section  
 exerts against the wall of the hole by an appropriate coefficient of  
 friction. A reasonable value for a coeff -- 4.2.1.2 Fluidic Drag.  
 Fluidic drag between the pipe and the viscous drilling fluid is  
 determined by multiplying the external surface area of the pipe by an  
 appropriate fluid drag coefficient. A reasonable value for a fluidic drag  
 coefficient is 0.0 -- 4.2.1.3 Effective Weight of Pipe. The effective  
 weight of the pipe is the unit weight of the pull section minus the unit  
 weight of any drilling fluid displaced by the pull section. This is  
 typically expressed in lb/ft. The unit weight of the pull s -- 4.2.2  
 Bending -- 4.2.3 External Pressure -- 4.3 Operating Loads -- 4.3.1  
 Internal Pressure -- 4.3.2 Bending -- 4.3.3 Thermal Expansion --  
 4.3.4 External Pressure -- 4.4 Pipe Material -- 4.5 Stresses in  
 Steel Pipe -- 4.5.1 Installation Stresses -- 4.5.1.1 Tensile Stress (  $f_t$  ).  
 The tension imposed on a circular pipe during installation by  
 HDD is assumed to act through the centroid of the cross section and  
 therefore is uniformly distributed over the cross section. The tensile  
 stress is det -- 4.5.1.2 Bending Stress (  $f_b$  ). Bending stress  
 resulting from a rigid steel pipe being forced to conform to the drilled  
 radius of curvature can be calculated using the following equation (   
 Young 1989 ): -- 4.5.1.3 External Hoop Stress (  $f_h$  ). Thin-  
 walled tubular members, such as steel pipes, fail by buckling or  
 collapse when under the influence of external hoop stress. A traditional  
 formula established by Timoshenko for calculation of the wall th.  
 4.5.1.4 Combined Installation Stresses. The greatest stress  
 condition for the pipe is typically located where the most serious  
 combination of tensile, bending, and external hoop stresses occurs  
 simultaneously. This is not always obvious in looking -- 4.5.2  
 Operating Stresses -- 4.5.2.1 Internal Hoop Stress (  $f_h$  ). Hoop  
 stress caused by internal pressure is calculated in Equation (4-20) (   
 ASME/ANSI 2010 ). -- 4.5.2.2 Bending Stress (  $f_b$  ). Bending  
 stresses are calculated and limited as shown in Section 4.5.1.2 . --  
 4.5.2.3 Thermal Stress (  $f_e$  ). The thermal stress resulting from  
 changes in pipe temperature from the point in time at which the pipe is  
 restrained by the surrounding soil to a typical operating condition is  
 calculated in Equation (4-21) ( AS -- 4.5.2.4 Combined Operating  
 Stresses. Hoop, thermal, and bending stresses imposed on the pipe  
 during operation should be combined and checked to evaluate the risk  
 of failure from combined stresses. This can be accomplished by  
 examining the maximum s -- 4.6 Stresses in a High-Density  
 Polyethylene Pipe and Fusible Polyvinyl Chloride Pipe -- 4.6.1  
 Installation Stresses -- 4.6.1.1 Tension. To determine whether a  
 given FPVC or HDPE pipe specification is sufficient to resist the tensile  
 loads encountered during HDD installation, a pulling load analysis  
 should first be performed to estimate the force required to pull the --  
 4.6.1.2 Bending. When installing an HDPE pipe by HDD, bending  
 stress is typically not critical. AWWA M55 ( AWWA 2020 ) states that an  
 HDPE pipe can be cold bent to a radius of 20 to 40 times the pipe  
 diameter (although experience has shown that HDD.  
 4.6.1.3 External Pressure. Another critical issue with the  
 installation of an HDPE pipe by HDD is the possibility of pipe collapse  
 owing to external pressure exerted by the drilling fluid in the annulus.

According to ASTM F1962 ( ASTM 2011b ), the -- 4.6.1.4 Mini-HDD. Small drill rigs (less than 25,000lb thrust) are often used to install small-diameter HDPE pipes. Typically, these bores are executed less conservatively than large crossings. They may contain more directional corrections, have | -- 4.6.2 Post-installation Stresses -- 4.6.2.1 Internal Pressure. AWWA C906 ( AWWA 1999 ) and ASTM F714 ( ASTM 2011a ) typically publish the internal pressure ratings of their products as a function of pipe dimension ratio (DR). These pressure ratings are based on the allowable hoop stre -- 4.6.2.2 External Pressure. If the maximum external pressure exceeds the minimum internal operating pressure, the pipeline is subjected to a differential external pressure equal to the difference between these pressures. This differential pressure s -- 4.6.2.3 Thermal. Following installation, an HDPE pipe segment should be cut to length only after reaching thermal equilibrium with the surrounding soil. A good practice is to overpull the pipe to allow for the contraction of an HDPE pipeline after -- 4.7 Ductile Iron Pipe Design Considerations -- 4.7.1 Installation Stresses -- 4.7.2 External Loads -- 4.8 Steel Pipe Corrosion Coating -- 4.8.1 Field Joint Coatings -- 4.8.2 Armoring Coatings -- References -- Chapter 5 : Construction Impacts -- 5.1 Introduction -- 5.2 Workspace -- 5.3 Drilling Fluid -- 5.3.1 Consumption and Characteristics -- 5.3.2 Containment and Recycling -- 5.3.3 Inadvertent Drilling Fluid Returns -- 5.3.4 Annular Seepage -- 5.3.5 Structural Failure by Piping -- 5.3.6 Drilling Fluid and Cuttings Disposal. 5.4 Surface Casing -- 5.5 Breakover Bends -- 5.6 Noise -- References -- Chapter 6 : As-Built Documentation -- 6.1 Introduction -- 6.2 Construction Staking -- 6.3 Documentation of Actual Drilled Path End points -- 6.4 Required Measurements prior to Commencing Drilling Operations -- 6.5 Pilot-Hole As-Built Calculations -- 6.6 Pilot-Hole Survey Data -- 6.6.1 Surface-Monitoring System -- 6.6.2 Gyroscopic Steering Tool -- 6.6.3 Walkover System -- 6.7 Pilot-Hole As-Built Error Distribution -- 6.8 Pilot-Hole As-Built Drawing -- 6.9 Post-Installation Survey -- References -- Glossary -- Index.

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## Sommario/riassunto

"MOP 108, third edition, addresses the design of major pipeline or duct segments to be installed by horizontal directional drilling (HDD)"--

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Nota di bibliografia	Includes bibliographical references and index.
Nota di contenuto	1 Introduction: Towards a Poetics of Displacement and Postmemory -- 2 Lived Religion, Displacement and Gender in Ludmila Ulitskaya's Daniel Stein, Interpreter -- 3 Remembering Childhood and Reassessing the Past in Elena Chizhova's The Time of Women -- 4 Voices of the Lost Experiences in Svetlana Alexievich's Secondhand Time. The Last of the Soviets -- 5 In Search of Memory in Maria Stepanova's In Memory of Memory -- 6 Conclusion: From Poetics to Politics of Displacement and

## Postmemory.

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### Sommario/riassunto

The book examines prominent literary works from the past two decades by Russian women writers dealing with the Soviet past. It explores works such as *Daniel Stein, Interpreter* by Ludmilla Ulitskaya, *The Time of Women* by Elena Chizhova, *Secondhand Time: The Last of the Soviets* by Svetlana Alexievich, and *In Memory of Memory* by Maria Stepanova, and uncovers connecting thematic structures and features. Focusing on the concepts of displacement and postmemory, the book shows how these works have given voice to those on the margins of society and of 'great history' whose resistance was often silent. In doing so, these women writers portray the everyday experiences and trauma of displaced women and girls during the second half of the twentieth century. This study offers new insights into the importance of these women writers' work in creating and preserving cultural memory in post-Soviet Russia. Marja Sorvari is Associate Professor of Russian Language and Culture at the University of Eastern Finland. She specializes in contemporary Russian literature and gender studies. She is author of *About the Self and the Time: On Autobiographical Texts* by Maria Arbatova, Elena Bonner, mma Gerštejn, Tamara Petkevi and Maija Pliseckaja (2004) and has co-edited several volumes.

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